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In re application of

TALBOT ALBERT CHUBB

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For: Process for Generating
Nuclear Heat

ART UNIT

3641

Examiner

Rick Palabrica

AMENDMENT

DETAILED DESCRIPTION

The new cold fusion process is a catalytic process in which surface and interface sciences are used to reduce the temperature at which exothermic reactions can take place. Catalysis substitutes configuration change for kinetic impact in promoting reaction. The configuration change employed is a coherent partitioning of the deuterium ion within an interface layer between a metal lattice and an ionic crystal. This change delocalizes deuteron charge density. Delocalization is the opposite of the process that increases charge density in muon-catalyzed fusion. Coherent partitioning creates a geometry that forbids emission of energetic neutrons, protons, and gamma rays. In addition, coherent partitioning adds lattice degrees of freedom to the product nucleus. The lattice geometry of the nucleus allows energy transfer to the hosting solid lattice via phonons. The process avoids strong inside-metal electric fields and deuteron acceleration. In the process a portion of a forced deuterium flow through a metal reactor makes contact with a salt-metal interface volume inside the reactor metal and undergoes a catalyzed configuration change and subsequent radiationless fusion reaction.

The apparatus supporting the process uses inside-metal structures
taught by Iwamura et al. Iwamura et al. constructed metal plate nuclear
reactors containing internal CaO-Pd metal interfaces. They have
demonstrated transmutation of surface Cs atoms into surface Pr atoms in
each of more than 50 experiments. They use clean deuterium flow methods
rather than electrolysis. Their Cs transmutations are equivalent to the
absorption of 4 deuterons by each surface Cs atom. The transmutations do
not to occur when normal hydrogen is substituted for deuterium, nor when
the internal interfaces between CaO crystal and Pd metal are not included
within the reactor. Since great cleanliness is maintained, since the
transmutation product covers a major fraction of the cesium-coated surface
of the reactor, and since sequential measurements show that the increase in
surface Pr matches the decrease in surface Cs, an explanation in terms of
contamination is unphysical. The transmutations have been repeated by
Higashiyama et al. at Osaka University.

The apparatus supporting the process uses solid electrolyte electrolysis
cells in contact with an Iwamura-type reactor plate to maintain and control a
continuous circulation of deuterium through the reactor plate at a higher flow
rate and higher D/Pd ratio than exists during the Iwamura et al. experiments.

The new process generates heat by exothermic nuclear reactions in
which deuterium participates, and uses solid state electrolysis device(s) that
deposit D atoms onto, and/or remove D atoms from a metal reactor plate
containing deuterium diffusion-impeding barriers. Deuterium that fails to
participate in a nuclear reaction during passage through the metal reactor
plate is re-circulated so as to maintain time-independed compositions, except
for a slow build-up of helium gas. The process can be carried out using a

number of alternate hardware assemblies. The Figures illustrate two such assemblies.

Now referring to Figures 1 and 2, pressure tight containment enclosure 1 is formed by aluminum, steel or other impervious metal, and contains an interior assembly comprising a flat permeable but non-porous metal reactor plate 2 interfacing on its left and right side planar surfaces with left and right layers of solid electrolyte 3. The reference characters in Figures 1 and 2 identify the right side components, but apply equally to the left side components. Both left and right layers of solid electrolyte 3 make surface contact with left and right permeable but non-porous metal foils 4. Reactor plate 2 is made of Pd. Now referring to Figure 3, within reactor plate 2 there is a left-side grouping of five layers 11 of CaO. The CaO layers are not shown in Figure 1. The CaO layer closest to the left surface of reactor plate 2 is located about 40 nm inward and parallel to the left planar surface of the plate. The layers of CaO are 2 nm thick. Within the grouping, the CaO-CaO layer separation is about 18 nm. The thickness, separation, and distance of the CaO layers from the closest metal surface of reactor plate 2 are as taught by Y. Iwamura, M. Sakano, and T. Itoh, Jpn. J. Appl. Phys. 41A, pp. 4642-4650, (2002), by Y. Iwamura, T. Itoh, M. Sakano, and S. Kuribayashi, in ICCF10 Abstracts, Presentation Tu15, (2003), and by T. Higashiyama, M. Sukano, H. Miyamaru, and A. Takahashi, ICCF10 Proceedings preprint, distributed through www.LENR-CANR.org, pp. 1-6, (2003). Iwamura et al. fabricated their test reactor plates, which have the desired internal layer construction, by starting with a plate of commercially pure Pd metal, coating the reactor plate with a sequence of five 2-nm layers of sputtered CaO, separated by four 18-nm layers of sputtered Pd metal, and topped with a 40-nm layer of sputtered Pd metal. The layers were deposited using argon ion beam

sputtering. Left and right solid electrolyte layers 3 are deposited layers of poly ethylene oxide (PEO), containing deuterided phosphoric acid, as taught by Biberian and G. Lonchamp, Proc. ICCF9 (2002), in "Condensed Matter Nuclear Science", ed. by Xing Z. Li (Tsinghua University Press, China, 2003) pp. 17-22. Each layer is about 1 mm thick and is a deuteron conductor. The hydrided version of the specified electrolyte has been used in the prior art in lithium batteries, where it operates between 70 °C and 120 °C. Left and right electrolyte layers 3 are each covered with a contacting piece of permeable but non-porous metal foil 4. Left and right metal foils 4 are made of Pd or Pd-alloy, and are about 0.1 mm thick. The rim surfaces of reactor plate 2, left and right electrolyte layers 3, and left and right metal foils 4 are held in place by annular rim insulator 5, which may be of poly tetrafluoroethylene plastic (PTFE). The left and right hermetically sealed feed-through insulators 6, which may be made of a ceramic, are sealed to left and right electrical wire leads 7. Left wire lead 7 makes contact with left metal foil 4, and right wire lead 7 makes contact with right metal foil 4. Left and right wire leads are made of Ni. The bottom wire lead 8 passes through feed-through insulator 14 and makes contact with reactor plate 2 by piercing the annular rim insulator 5, as shown in Figures 1 and 2. Bottom wire lead 8 is made of Ni. It supports the sub-assembly consisting of reactor plate 2, left and right electrolyte layers 3, left and right metal foils 4, and annular rim insulator 5. Gas supply tube 12 pierces a wall of containment enclosure 1, and is used to fill containment vessel 1 with D₂ gas prior to use, and to furnish pre-operation conditioning D₂ gas which is absorbed by the metal components during conditioning of the system prior to process operation. Square box 13 schematically represents a pressure transducer that produces an electrical

output voltage which measures gas pressure inside pressure tight vessel enclosure 1.

Prior to process operation, containment vessel 1 is filled with D_2 gas and is heated to above about $70^\circ C$. During process operation, wire lead 8 may be connected to ground electrical potential, which is defined as reference potential $V = 0$ volts. Left metal foil 4, left solid electrolyte layer 3, and left surface of metal plate 2 form a left electrolysis cell. The left electrolysis cell is the inflow electrolysis cell. Right metal foil 4, right solid electrolyte layer 3, and right surface of metal plate 2 form a right electrolysis cell. The right electrolysis cell is the outflow electrolysis cell. Left wire lead 7 is connected to an external power supply providing an electrical potential V_L , which is positive relative to the left cell zero-current cell potential V_{Lo} , thereby polarizing the left cell so as to drive a deuterium permeation flow toward the right. Right wire lead 7 is connected to an external power supply providing an electrical potential V_R , which is negative relative to the right cell zero-current cell potential V_{Ro} , thereby polarizing the right cell so as to drive a deuterium permeation flow also toward the right. As taught by Biberian and Lonchampt, current flow through left electrolyte removes deuterium dissolved in left metal foil 4 and deposits deuterium onto metal plate 2, which absorbs the deposited deuterium. As taught by Biberian and Lonchampt, left-to-right current flow through right electrolyte 3 desorbs deuterium from metal plate 2 and deposits deuterium onto right metal foil 4, which absorbs the deuterium. Concurrently D_2 gas adsorbs and dissociates on the left surface of left metal foil 4 and desorbs from the right surface of right metal foil 4 into the gas. After metal conditioning and during operation the composition of both left and right electrolytic layers 3 stays constant since inflow deuterium balances outflow deuterium.

During process operation, absorption of deuterium on the left surface of reactor plate 2 and concurrent desorption of deuterium from the right side of reactor plate 2 drives a left-to-right permeation flow of deuterium through reactor plate 2. This permeation flow resembles that used in the studies by Iwamura et al. (2002 and 2003) and Higashiyama et al. (2003), which studies have demonstrated deuterium participation in exothermic nuclear reactions.

Although theory and conjecture are not part of the description of the apparatus and process, the description is aided by summarizing the science that seems to explain the Iwamura et al. and Higashiyama et al. results. In "The dd Cold Fusion-Transmutation Connection" by T. A. Chubb, ICCF10 Proceedings preprint, distributed through www.LENR-CANR.org, pp. 1-15, (2003a), a quantum mechanics wave equation-wave function model explains how the prescribed permeation flow leads to exothermic nuclear reactions. Quantum mechanics coordinate exchange replaces quantum mechanics tunneling in the reaction model.

Modeling of the process assumes that impeded deuterium permeation flow creates a nuclearly active configuration of wavelike deuterium, which behaves much like the conduction electron medium in a metal. Quantum mechanics uses the term "Bloch function" to describe the nuclearly-active condensed-matter deuterium configuration. The conduction electrons in a metal have a similar delocalized wavelike form and provide a low resistance conduction current flow in response to a voltage potential difference across a metal crystal. Similarly, wavelike deuterium provides a low resistance deuterium conduction permeation flow in response to a difference in the chemical potential of wavelike deuterium across a metal crystal.

The total deuterium permeation flow is modeled as being partitioned between a relatively large diffusion flow of non-nuclearly-active interstitial

deuterium within the metal and a relatively small conduction flow carried by nuclearly-active wavelike deuterium. The normal form of deuterium in a metal is the non-nuclearly-active interstitial configuration. The normal diffusion flow is driven by a concentration gradient of deuterium in self-trapping potential wells. The normally occupied potential wells in Pd metal are known to be centered on the octahedral sites of the face-centered cubic (fcc) metal lattice. The conduction flow is modeled as being carried by wavelike deuterons occupying shallower, non-self-trapping potential wells. These wells are believed to be centered on the tetrahedral sites of the fcc metal lattice, as explained in "LENR: Superfluids, Self-Trapping and Non-Self-Trapping States", T. A. Chubb, ICCF10 Proceedings preprint, distributed through www.LENR-CANR.org, pp. 1-4, (2003b). At each of the CaO diffusion-impeding layers there is a scattering of both types of deuterium. The scatterings are modeled as reversible scatterings of individual deuterons between self-trapping and non-self-trapping sites. Reversibility requires that a fraction of the normally diffusing deuterons scatter into wavelike deuterons when they cross a diffusion-impeding layer. The resulting wavelike deuterons in the non-self-trapping sites are the nuclearly reactive component which, in the Iwamura et al. studies, spreads out and participates in exothermic nuclear reactions on the metal surface, releasing heat. The nuclear reactions demonstrated by Iwamura et al. and Higashiyama et al. are $^{133}\text{Cs} + 8\text{D} \rightarrow ^{141}\text{Pr} + 50.5 \text{ MeV}$ and $^{88}\text{Sr} + 8\text{D} \rightarrow ^{96}\text{Mo} + \sim 53.5 \text{ MeV}$.

A second implementation of the process uses adsorption of gas directly onto the inflow surface of reactor plate 2 as the first step of a deuterium recirculation loop which includes passage of deuterium through reactor plate 2. Now referring to Figure 4, pressure tight containment enclosure 1 contains an interior assembly designed to provide an upward

deuterium permeation flow through reactor plate 2. In Figure 4, reactor plate 2 is coated on its annular rim surface by insulator coating 9. Annular insulator coating 9 is made of a non-porous material such as PTFE. Reactor plate 2 is made of Pd metal and contains internally a grouping of diffusion-impeding CaO layers near its bottom planar surface, the internal layers are configured as described in Figure 3. Reactor plate 2 is supported from the bottom surface of containment enclosure 1 by metal cylinder 10, which is of lesser diameter than reactor plate 2. As a result, a portion of the bottom surface of reactor plate 2 is exposed to D_2 gas within containment enclosure 1 during process operation. Reactor plate 2 makes contact with, and is covered by, solid electrolyte layer 3. Solid electrolyte layer 3 is made of poly ethylene oxide containing deuterided phosphoric acid. Solid electrolyte layer 3 makes contact with and is covered by metal foil 4, which is made of Pd metal. Metal foil 4 is positioned by annular positioning fixture 15, which is made of PTFE. The top surface of reactor plate 2, solid electrolyte layer 3, and metal layer 4 constitute an outflow electrolysis cell. Containment enclosure 1 is made of metal and is connected to electrical ground potential, designated $V = 0$ volts. Wire lead 7, which is made of Ni, passes through feed-through insulator 6 to make contact with metal foil 4. During process operation, wire lead 7 is connected externally to an electrical power supply that keeps metal foil 4 at a potential V which is more negative than the zero-current cell potential V_0 .

During process operation as implemented using the assembly configuration of Figure 4, D_2 gas within containment vessel enclosure 1 dissociates on the exposed portion of the bottom surface of reactor plate 2. It is known from the prior art that D_2 gas dissociates into atom form when adsorbed onto clean Pd-like metals. The resulting surface atoms are absorbed into the metal of reactor plate 2. At the top surface of reactor plate

2, surface deuterium desorbs from reactor plate 2 and enters solid electrolyte 3 as deuterium ions. With the potential of metal foil maintained at $V < V_o$, D^+ ion current flows through solid electrolyte 3 and deuterium is absorbed into the bottom surface of metal foil 4. Deuterium desorbs from the top surface of metal foil 4 as D_2 gas, completing the deuterium recirculation loop. The resulting upward permeation flow through reactor metal 2 creates nuclearly active deuterium as previously described.

Again referring to Figure 4, a third implementation of the process uses the assembly of Figure 4 but imposes a reverse electrical polarization of solid-electrolyte layer 3. The reverse polarization reverses the direction of deuterium circulation. The potential of metal foil 4 is maintained at $V > V_o$. D_2 gas within containment vessel enclosure 1 dissociates on the top surface of reactor plate 4, and desorbs downward into solid-electrolyte layer 3. Solid-electrolyte layer 3 functions as the electrolyte of an inflow electrolysis cell. Deuterium plating out of the electrolysis cell deposits onto the top surface of reactor plate 2 and dissolves into the bulk metal. The downward flowing deuterium is subject to scattering. Most of the inflowing deuterium desorbs from the bottom surface of reactor plate 2 as D_2 gas, completing the recirculation process. Optionally, the grouping of CaO layers may be near the top, middle, or bottom of reactor plate 2. In this third implementation of the process, the process takes place at a higher deuterium chemical potential and with a smaller deuterium gradient within the reactor plate than in the second implementation of the process, using the same assembly hardware.

Three additional implementations of the process are identical to the three implementations described above, except that they use a different internal diffusion-impeding structure within reactor plate 2. Instead of using thin non-metallic diffusion-impeding layers, the processes use an internal

dispersion of salt-like non-metallic inclusions within reactor plate 2 as means for scattering nuclearly non-reactive diffusing deuterium into the nuclearly reactive configuration. Using a distribution of non-metallic inclusions resembling fragments of the diffusion-impeding CaO layers is within the scope of the invention provided that the impeding of deuterium permeation flow is sufficient to scatter amounts of deuterium into the nuclearly reactive state that are comparable to or greater than the amounts achieved by Iwamura et al. (2002).

In other options the process replaces uni-directional deuterium permeation flows within reactor plate 2 with back-and-forth deuterium permeation flow, by using a power supply or supplies that repeatedly alternate the potentials applied to wire leads(s) 7 between values more positive and less positive than the zero-current cell potentials.

Many modifications and variations of the assembly hardware supporting process operation are possible in light of the above teachings. Among these is that of replacing the planar sequence of component layers with a cylindrical sequence of the same functional elements. Also, it is well known in the art of fuel cell technology and in the physics of metal-hydrogen systems that one can coat a metal's surface with fine Pd powder or Pd-Ag alloy powder, thereby increasing the effective surface area for absorption of hydrogen into the metal's bulk. Also, it is well known in prior art that use of Pd coatings on a metal's de-oxidized surface can permit absorption of hydrogen into a metal's bulk for metals which form oxides that otherwise block absorption of hydrogen. Use of such surface treatments on the metal foil(s) and/or on the reactor plate, and use of metals other than Pd or Pd alloys for the foil(s) and/or reactor plate within the assembly should be considered as within the scope of the invention. Furthermore, use of internal

non-metallic layers made of materials other than CaO within a reactor plate have been taught by Iwamura et al. The number, placement, uniformity, and thickness of the internal non-metallic layers can be widely varied provided that deuterium permeation is not prevented, and provided that the impeding of the deuterium permeation flow is sufficient to scatter amounts of deuterium into the nuclearly reactive state that are comparable to, or greater than the amounts achieved by Iwamura et al. (2002). For example, inclusion of both a left and right grouping of diffusion-impeding layers could be used with back and forth deuterium permeation flow through reactor plate 2 of Figure 1. Addition of voltage control circuitry using signals from pressure transducer 13 together with temperature readings as a basis for setting the electrolysis cell voltages should be considered as within the scope of the invention. The invention can also be used in conjunction with various laser and acoustic stimulation devices, such as are being used as enhancers in cold fusion test devices. It is therefore to be understood that within the scope of the appended claims the invention may be practiced otherwise than as specifically described.

Respectfully submitted,



Melvin L. Crane
Reg. No. 18212

318 S. Cleveland St.
Arlington VA 22204
Date- ~~10/18/05~~ 10/18/05
telephone 703 521 9022